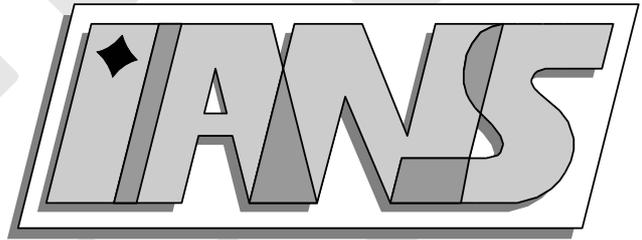


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to nonlinear acoustic-structure interaction

Roland Ernst, Bernd Flemisch and Barbara Wohlmuth

**Berichte aus dem Institut für
Angewandte Analysis und Numerische
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Abstract

A new Schwarz method for nonlinear systems is presented, constituting the multiplicative variant of a straight forward additive scheme. Local convergence can be guaranteed under suitable assumptions. The scheme is applied to nonlinear acoustic-structure interaction problems. Numerical examples validate the theoretical results. Further improvements are discussed by means of introducing overlapping subdomains and employing an inexact strategy for the local solvers.

We present a new Schwarz type domain decomposition method for nonlinear problems. Such methods typically lead to schemes where an outer iteration for the subproblem connection and an inner subspace iteration on each subproblem have to be applied, [14, 16, 17]. Our method constitutes, by means of a Gauß-Seidel type outer iteration, a multiplicative variant of the straight forward additive scheme introduced in [9], and further refined in [1, 6].

In Section 1, we first repeat the general setting and the theoretical results of the additive Schwarz method for nonlinear problems. Based on this framework, we introduce and analyze the corresponding multiplicative version. In the subsequent sections, the domain decomposition scheme is applied to nonlinear acoustic-structure interaction problems. In particular, we extend the elasto-acoustic problem formulation of [10] to geometrically nonlinear structures, [8], and nonlinear acoustic wave propagation, [13]. After introducing the single field problems in Section 2, we present the coupled problem formulation in Section 3, yielding two illustrative numerical schemes using different solvers for the subproblems, a Newton-like and a fixed point iteration scheme. We finally present the results of several numerical examples in Section 4. First, the theoretical results are validated and the convergence behavior of the additive and the multiplicative variant are compared. Moreover, further possible improvements of the scheme are discussed, one by the introduction of a small subregion where both subdomains overlap, and another by employing an inexact strategy for the local linear solver.

1 Two Schwarz methods for nonlinear problems

The system we want to investigate is

$$F(u^*) = \begin{pmatrix} F_e(u^*) \\ F_a(u^*) \end{pmatrix} = 0, \quad (1)$$

where F_e and F_a stand for the elastic and acoustic subproblems, respectively. We remark that this specific decomposition is purely motivated by the application presented afterwards, and that the theoretical results presented here in this section are general and do not depend on the physical origin of the subproblems. Moreover, our results can be extended to the case of more than two subproblems, and we will clearly indicate how this can be done.

A major reason for the potential efficiency of our approach, even in the two-subdomain case, is that often only one part of the problem equations is nonlinear.

In the sequel, we assume that the elastic part F_e is nonlinear and the acoustic part F_a is linear. Thus, we can exploit the structure of system (1) by constructing iterative schemes, where the nonlinear equations are decoupled from the linear ones in each iteration step. The choice of the nonlinearity in the elastic part is arbitrary and an adaption to the other case can easily be done by changing the role of the indices. In the first part, we present the most straightforward alternative by means of a non-overlapping block Jacobi scheme and repeat the results provided by [9]. Second, we additionally introduce a multiplicative variant of the scheme yielding an improved convergence behavior.

1.1 A nonlinearly preconditioned Richardson scheme

We apply an additive scheme within the framework of nonlinear domain decomposition methods provided by [9], and borrow the notation and the ideas from [1, 6]. Indicating with m the global dimension of the system (1), we partition the set $\{1, \dots, m\}$ into the index sets I_e and I_a corresponding to the structural and to the acoustic degrees of freedom, respectively, and set $m_i = |I_i|$, $I_i = \{i_1, \dots, i_{m_i}\}$, $i = e, a$. Defining the prolongation matrices $E_i^T \in \mathbb{R}^{m \times m_i}$ and the restriction matrices $E_i \in \mathbb{R}^{m_i \times m}$ by

$$(E_i)_{k\ell} = \begin{cases} 1, & \ell = i_k, \\ 0, & \text{else,} \end{cases} \quad i = e, a,$$

we set $P_i = E_i^T E_i \in \mathbb{R}^{m \times m}$, and define the subspaces V_e and V_a by $V_i = P_i \mathbb{R}^m$. For the different parts we have $F_i = P_i F$. Given $v \in \mathbb{R}^m$, the correction $T_i(v) \in V_i$ is defined as the solution of the subspace problem

$$F_i(v - T_i(v)) = 0, \quad i = e, a. \quad (2)$$

For the structural part, this subspace problem is nonlinear and will be solved by Newton's method. However, for the acoustic part, (2) gives the usual linear subspace correction

$$T_a(u) = E_a^T (K_a^*)^{-1} E_a F_a(u).$$

In the spirit of [6], we introduce a new function

$$\mathcal{F}(u) = T_e(u) + T_a(u),$$

referred to as nonlinearly preconditioned $F(u)$, and attempt to solve

$$\mathcal{F}(u^*) = 0 \quad (3)$$

instead of (1). The solvability of the subproblems (2) and the equivalence of the two nonlinear systems (1) and (3) are stated in the following theorem which is proved in [6] using the results from [9].

Theorem 1.1 ([6, 9]). *Let the following assumptions be satisfied:*

(A1) *The Jacobian $J(u) = F'(u)$ exists and is continuous in a neighborhood D of the exact solution u^* .*

(A2) *The matrix $J(u^*)$ is nonsingular.*

(A3) *The matrices $E_i J(u^*) E_i^T$ are nonsingular.*

Then, the subproblems (2) are all uniquely solvable in a neighborhood of u^ in D . Moreover, the nonlinear systems (1) and (3) are equivalent in the sense that they have the same solution in a neighborhood of u^* in D .*

It remains to solve the preconditioned system (3). As suggested by [9], we employ a standard Richardson iteration, namely, given $u^{(k)}$ and a damping parameter ω , we calculate in each iteration step

$$u^{(k+1)} = \Phi(u^{(k)}), \text{ with } \Phi(u) = u - \omega \mathcal{F}(u). \quad (4)$$

The expected convergence rate of (4) can be given in terms of the linearized problem $Au - b = 0$ with $A = J(u^*)$, $b = Au^*$. In this case, the subspace iteration (4) reduces to the well-known linear additive Schwarz method, [17], with the iteration matrix

$$M_\omega = I - \omega \sum_{i=e,a} E_i^T A_i^{-1} E_i A, \quad A_i = E_i A E_i^T.$$

Assuming

$$\|M_\omega\| \leq \zeta < 1, \quad (A4)$$

the convergence behavior is described by the following theorem.

Theorem 1.2 ([9]). *Assume (A1)-(A4), and let $\zeta' \in (\zeta, 1)$. Then there is a neighborhood $D(\zeta')$ of u^* such that*

$$\|\Phi(v) - \Phi(w)\| \leq \zeta' < 1, \quad v, w \in D,$$

i.e., the nonlinear subspace iteration (4) converges in D and has the same asymptotic convergence rate ζ as the linear iteration applied to the linearized equations.

Remark 1.3. One possible improvement is to replace the simple Richardson iteration in (4) by an inexact Newton method. This yields so-called ASPIN methods, i.e., Additive Schwarz Preconditioned Inexact Newton methods. They have been introduced in [6], and a proof of locally quadratic convergence under essentially the same assumptions (A1)-(A3) is provided in [1]. Here, we will present an alternative way.

1.2 A multiplicative preconditioner

In contrast to the nonlinearly preconditioned system (3), referred to as additive or Jacobi variant in the sequel, we can define a multiplicative or Gauß–Seidel variant by setting

$$\mathcal{F}_m(u) = T_e(u) + T_a(u - T_e(u)). \quad (5)$$

Similar to (3), we now try to solve the nonlinearly preconditioned system

$$\mathcal{F}_m(u^*) = 0. \quad (6)$$

To the best knowledge of the authors, no theory for this multiplicative type of nonlinear subspace preconditioning exists. In order to analyze this case, we first need the following lemma.

Lemma 1.4. *Under Assumptions (A1)–(A3), the Jacobian $\mathcal{J}(u) = \mathcal{F}'_m(u)$ is nonsingular in a neighborhood of u^* .*

Proof. Setting $\bar{u} = u - T_e(u)$ and applying the chain rule, we have that

$$\mathcal{J}(u) = I - (I - T'_a(\bar{u}))(I - T'_e(u)).$$

We follow the argumentation for the additive case from [1, 6]. There, it is shown that

$$T'_i(u) = J_i^{-1}(u - T_i(u))J(u - T_i(u)),$$

where $J_i^{-1}(u - T_i(u))$ is understood as the subdomain inverse, i.e., $J_i^{-1}(u - T_i(u)) = E_i^T(E_i J_i(u - T_i(u))E_i^T)^{-1}E_i$, which is known to exist by Assumption (A3). By continuity arguments, $J(u - T_i(u))$ and $J(\bar{u} - T_i(\bar{u}))$ are close to $J(u)$ in a neighborhood of u^* . From the same arguments it follows that the matrices

$$B(u) = I - (I - J_a^{-1}(u)J(u))(I - J_e^{-1}(u)J(u))$$

and $\mathcal{J}(u)$ are continuous in a neighborhood of u^* , and that

$$\lim_{u \rightarrow u^*} \mathcal{J}(u) = \lim_{u \rightarrow u^*} B(u) = \mathcal{J}(u^*). \quad (7)$$

In the present simple case of a decomposition into two nonoverlapping sets, it is easy to explicitly construct the inverse $B^{-1}(u)$ in terms of the subdomain Jacobians. In particular, if we omit the dependence on u for the moment, it is easy to see that

$$B = \begin{pmatrix} J_e^{-1} & 0 \\ J_a^{-1} J_{ae} J_e^{-1} & J_a^{-1} \end{pmatrix} J,$$

and, therefore,

$$B^{-1} = J^{-1} \begin{pmatrix} J_e & 0 \\ -J_{ae} & J_a \end{pmatrix}.$$

Using the regularity of $B(u)$, the observation (7), and continuity, we obtain the desired regularity of $\mathcal{J}(u)$ close to u^* . \square

Remark 1.5. The generalization of the proof given above to the case of many nonoverlapping subsets is straightforward. However, in presence of overlap, the proof of the regularity of $B(u)$ remains to be given.

Concerning the equivalence of (1) and (6), we show the following result in analogy to Theorem 1.1.

Theorem 1.6. *Under Assumptions (A1)-(A3) from Theorem 1.1, the nonlinear systems (1) and (6) are equivalent in the sense that they have the same solution in a neighborhood of u^* in D .*

Proof. We follow the lines of the proof of Theorem 1.1 provided in [6]. Assuming that u^* solves (1), we have $F_i(u^*) = 0$, $i = e, a$. Comparing this with the definition of T_i in (2), and using the local unique solvability guaranteed by Theorem 1.1, we have $T_i(u^*) = 0$. Therefore, u^* is also a solution of (6). It remains to show that u^* is unique in a local neighborhood. By Lemma 1.4, the Jacobian $\mathcal{F}'_m(u^*)$ is nonsingular, and therefore, according to the inverse function theorem, the solution is locally unique. \square

In order to solve (6), we apply the Richardson iteration (4) with \mathcal{F} replaced by \mathcal{F}_m , namely,

$$u^{(k+1)} = \Phi_m(u^{(k)}), \text{ with } \Phi_m(u) = u - \omega \mathcal{F}_m(u). \quad (8)$$

We expect that an analogue of Theorem 1.2 has to hold, i.e., the convergence rate should be close to the one of the corresponding linear iteration applied to the linearized problem. In particular, the Richardson iteration in the linear case described above reduces to the standard multiplicative Schwarz method with the iteration matrix

$$M_{\omega, m} = I - \omega \left(I - \prod_{i=e, a} (I - E_i^T A_i^{-1} E_i A) \right).$$

Analogous to (A4), we now assume that

$$\|M_{\omega, m}\| \leq \zeta < 1. \quad (\text{A4}')$$

Theorem 1.7. *Assume (A1)-(A3), (A4'), and let $\zeta' \in (\zeta, 1)$. Then there is a neighborhood $D(\zeta')$ of u^* such that*

$$\|\Phi_m(v) - \Phi_m(w)\| \leq \zeta' < 1, \quad v, w \in D.$$

i.e., the nonlinear subspace iteration (8) converges in D and has the same asymptotic convergence rate ζ as the linear iteration applied to the linearized equations.

Proof. We alternate the proof of Theorem 1.2 presented in [9]. There, the analysis is based on weaker assumptions employing a general difference quotient DF . Since (A1) is satisfied, we can choose $DF(u', u'') \in \mathbb{R}^{m \times m}$ as

$$DF(u', u'') = \int_0^1 J(u' + t(u'' - u')) dt.$$

In [9], it is shown that

$$T_i(u') - T_i(u'') = DT_i(u', u'')(u' - u''), \quad (9)$$

for all u', u'' sufficiently close to u^* , where $DT_i(u', u'')$ is defined as

$$DT_i(u', u'') = E_i^T (E_i DF E_i^T)^{-1} E_i DF, \quad DF = DF(u' - T_i(u'), u'' - T_i(u'')).$$

Moreover, $DT_i(u', u'')$ satisfies

$$DT_i(u', u'') \rightarrow J_i^{-1}(u^*) J(u^*) \quad \text{as } u', u'' \rightarrow u^*. \quad (10)$$

In view of (5), and starting from u', u'' , we set $\bar{u} = u' - T_e(u')$, $\hat{u} = u'' - T_e(u'')$, and derive from (9) the relation

$$\begin{aligned} T_a(\bar{u}) - T_a(\hat{u}) &= DT_a(\bar{u}, \hat{u})(\bar{u} - \hat{u}) \\ &= DT_a(\bar{u}, \hat{u})(u' - u'' - (T_e(u') - T_e(u''))) \\ &= DT_a(\bar{u}, \hat{u})(I - DT_e(u', u''))(u' - u''). \end{aligned} \quad (11)$$

The definition (5) of \mathcal{F}_m yields

$$\Phi_m(u') - \Phi_m(u'') = (u' - u'') - \omega((T_e(u') - T_e(u'')) + (T_a(\bar{u}) - T_a(\hat{u}))),$$

and inserting (9) and (11), we have

$$\Phi_m(u') - \Phi_m(u'') = \left(I - \omega \left(I - (I - DT_a(\bar{u}, \hat{u}))(I - DT_e(u', u'')) \right) \right) (u' - u'').$$

Employing (10) and the fact that $\bar{u}, \hat{u} \rightarrow u^*$ as $u', u'' \rightarrow u^*$, we see that

$$I - \omega \left(I - (I - DT_a(\bar{u}, \hat{u}))(I - DT_e(u', u'')) \right) \rightarrow M_{\omega, m} \quad \text{as } u', u'' \rightarrow u^*.$$

Therefore, (A4') implies the desired assertion. \square

Remark 1.8. By using induction arguments, the proof of Theorem 1.7 can easily be generalized to the case of many subdomains.

Remark 1.9. As mentioned in Remark 1.3, a further improvement could be achieved by employing an inexact Newton method instead of the Richardson scheme 8, yielding a multiplicative variant of ASPIN methods, [1, 6]. This clearly is subject of our future work.

2 Model equations

In the following two application-oriented sections of this paper we derive the different nonlinear subproblems of system (1) in order to apply the theoretical results. The field of fluid-structure interactions contains many applications for elasto-acoustic coupling problems, especially nonlinear ones. Linear elasticity is restricted to the case of small deformations. Nonlinear acoustic effects including dissipation and generation of higher harmonics play an important role in ultrasonics. The choice of a velocity potential or pressure based formulation for the acoustic part and of a displacement one of the elastic part results in Dirichlet–Neumann type interface conditions. We start with introducing the single field problems of elasto-dynamics and of acoustics, providing the strong and weak continuous formulations.

2.1 Nonlinear structural dynamics

We investigate the deformation of an elastic body $\Omega^e \subset \mathbb{R}^d$ with density $\rho_e : \Omega^e \rightarrow \mathbb{R}$ under given time dependent volume and surface forces \mathbf{f} and \mathbf{g} . The boundary of Ω^e with unit normal vector \mathbf{n}_e is the union of disjoint subsets Γ_N^e and Γ_D^e , on which natural and essential data are given, respectively. If the strains remain small but the deformations become large, one has at least to consider the geometrically nonlinear elasticity setting. This amounts to using the full Green–St. Venant tensor

$$E = \frac{1}{2}(F^T F - \text{Id}) = \frac{1}{2}(C - \text{Id}), \quad (12)$$

with $F = \text{Id} + \text{grad } \mathbf{u}$ the deformation gradient and $C = F^T F$ the right Cauchy–Green strain tensor. We have the constitutive law

$$S = \lambda_L(\text{tr } E)\text{Id} + 2\mu_L E = \mathcal{C}E, \quad (13)$$

defining the second Piola–Kirchhoff stress tensor S , with \mathcal{C} the Hooke-tensor and the Lamé constants λ_L, μ_L . The strong formulation for elasto-dynamic problems then reads as follows: given $\mathbf{u}_0, \mathbf{u}_1, \mathbf{f} : \Omega^e \rightarrow \mathbb{R}^d$, find $\mathbf{u} : \Omega^e \times (0, T) \rightarrow \mathbb{R}^d$ such that

$$\rho_e \mathbf{u}_{tt} - \text{div}(FS) = \mathbf{f} \quad \text{in } \Omega^e \times (0, T), \quad (14a)$$

complemented by the boundary conditions

$$\mathbf{u} = \mathbf{0} \quad \text{on } \Gamma_D^e \times (0, T), \quad FS\mathbf{n} = \mathbf{g} \quad \text{on } \Gamma_N^e \times (0, T), \quad (14b)$$

and initial conditions

$$\mathbf{u}(\cdot, 0) = \mathbf{u}_0, \quad \mathbf{u}_t(\cdot, 0) = \mathbf{u}_1 \quad \text{in } \Omega^e. \quad (14c)$$

Under additional assumptions on the data, it is possible to establish the well-posedness of (12)–(14c), cf. [8], [15]. For the weak formulation, it is natural to use the space

$$X^e = (H_{\Gamma_D^e}^1(\Omega^e))^d = \{\mathbf{v} \in (H^1(\Omega^e))^d : \gamma_0 \mathbf{v} = \mathbf{0}\}$$

where $\gamma_0 : (H^1(\Omega^e))^d \rightarrow (H^{1/2}(\Gamma_D^e))^d$ denotes the usual trace operator. We employ the standard setting of Sobolev spaces for evolution problems, the space $L^2(0, T; X)$ consists of functions $t \mapsto v(t)$ which are Lebesgue-measurable on $(0, T)$ with respect to the measure dt , such that

$$\|v\|_{L^2(0, T; X)} = \left(\int_0^T \|v(t)\|_X^2 dt \right)^{1/2} < \infty.$$

The resulting variational problem reads:

find $\mathbf{u} \in L^2(0, T; X^e)$, $\dot{\mathbf{u}} \in L^2(0, T; L^2(\Omega^e))$, and $\ddot{\mathbf{u}} \in L^2(0, T; H^{-1}(\Omega^e))$ such that for all times $t \in (0, T)$

$$\langle \rho_e \ddot{\mathbf{u}}, \mathbf{v} \rangle_{\Omega^e} + a_e(\mathbf{u}, \mathbf{v}) = l_e(\mathbf{v}) = (\mathbf{f}, \mathbf{v})_{\Omega^e} + (\mathbf{g}, \mathbf{v})_{\Gamma_N^e}, \quad \mathbf{v} \in X^e, \quad (15)$$

together with initial conditions (14c). In (15), $\langle \cdot, \cdot \rangle_{\Omega^e}$ indicates the duality product on $X^e \times (X^e)'$. Transforming to the weak setting, the nonlinearity in (12) results in the fact that $a_e(\cdot, \cdot)$ is nonlinear in the first and linear in the second argument, i.e., $a_e(\mathbf{u}, \mathbf{v}) = \sum_{i=1}^4 a_{e,i}(\mathbf{u}, \mathbf{v})$, is given by, cf. [8],

$$\begin{aligned} a_{e,1}(\mathbf{u}, \mathbf{v}) &= (\mathcal{C}\varepsilon(\mathbf{u}), \varepsilon(\mathbf{v}))_{\Omega^e}, & a_{e,2}(\mathbf{u}, \mathbf{v}) &= \frac{1}{2}(\mathcal{C} [(\text{grad } \mathbf{u})^T \text{grad } \mathbf{u}], \text{grad } \mathbf{v})_{\Omega^e}, \\ a_{e,3}(\mathbf{u}, \mathbf{v}) &= (\text{grad } \mathbf{u} \mathcal{C} \text{grad } \mathbf{u}, \text{grad } \mathbf{v})_{\Omega^e}, & a_{e,4}(\mathbf{u}, \mathbf{v}) &= \frac{1}{2}(\text{grad } \mathbf{u} \mathcal{C} [(\text{grad } \mathbf{u})^T \text{grad } \mathbf{u}], \text{grad } \mathbf{v})_{\Omega^e}, \end{aligned}$$

with the linearized strain tensor

$$\varepsilon(\mathbf{u}) = \frac{1}{2}(\text{grad } \mathbf{u} + [\text{grad } \mathbf{u}]^T).$$

2.2 Linear structure dynamics

Assuming small deformations and small strain, it is sufficient to investigate the linear system

$$\rho_e \mathbf{u}_{tt} - \text{div}(\sigma) = \mathbf{f} \quad \text{in } \Omega^e \times (0, T),$$

with the stress tensor σ given by Hooke's Law

$$\sigma = \lambda_L(\text{tr } \varepsilon)\text{Id} + 2\mu_L \varepsilon,$$

complemented by the boundary conditions

$$\mathbf{u} = \mathbf{0} \quad \text{on } \Gamma_D^e \times (0, T), \quad \sigma \mathbf{n} = \mathbf{g} \quad \text{on } \Gamma_N^e \times (0, T),$$

and initial conditions (14c). The weak form is analogous to (15) with $a_e(\cdot, \cdot)$ replaced by $a_e^{\text{lin}}(\cdot, \cdot) = a_{e,1}(\cdot, \cdot)$.

2.3 Nonlinear acoustic waves

For the description of the acoustic wave propagation within a domain $\Omega^a \subset \mathbb{R}^d$, we use the wave equation for the velocity potential ψ , i.e., $\mathbf{v}_a = -\nabla\psi$ with \mathbf{v}_a denoting the acoustic velocity field. The acoustic pressure p_a is then related to the acoustic velocity potential ψ by

$$p_a = \rho_a \psi_t \quad (16)$$

with $\rho_a : \Omega^a \rightarrow \mathbb{R}$ the mean density of the fluid. This connection will be important for an interface condition of force transition in the coupled system. Indicating with $c : \Omega^a \rightarrow \mathbb{R}$ the speed of sound, the acoustic problem with the nonlinear wave equation derived by Kuznetsov [13] reads as follows:

given $\psi_0, \psi_1 : \Omega^a \rightarrow \mathbb{R}$, find $\psi : \Omega^a \times (0, T) \rightarrow \mathbb{R}$ such that

$$\frac{1}{c^2} \psi_{tt} - \Delta\psi = \frac{1}{c^2} \frac{\partial}{\partial t} \left(b \Delta\psi + \frac{1}{c^2} \frac{B}{2A} \psi_t^2 + (\nabla\psi)^2 \right) \quad \text{in } \Omega^a \times (0, T), \quad (17a)$$

with boundary conditions

$$\psi = 0 \quad \text{on } \Gamma_D^a \times (0, T), \quad \nabla\psi \cdot \mathbf{n}_a = g \quad \text{on } \Gamma_N^a \times (0, T), \quad (17b)$$

and initial conditions

$$\psi(\cdot, 0) = \psi_0, \quad \psi_t(\cdot, 0) = \psi_1 \quad \text{in } \Omega^a. \quad (17c)$$

The parameter b involves thermodynamical effects as well as the viscosity of the fluid, whereas B/A is called the nonlinearity parameter of the fluid. From a modeling point of view one could extend (16) to a higher accuracy relation $p_a = \rho_a(\psi_t + \frac{1}{2}(\nabla\psi)^2 - \frac{1}{2c^2}\psi_t^2)$, [11], which would lead to a different force interface condition. But the occurrence of the nonlinear effects depends only on the nonlinear wave equation (17a). Due to this fact we consider here condition (16). Setting $X^a = H_{\Gamma_D^a}^1(\Omega^a)$, the weak form of (17) reads:

find $\psi \in L^2(0, T; X^a)$, $\dot{\psi} \in L^2(0, T; L^2(\Omega^a))$, and $\ddot{\psi} \in L^2(0, T; H^{-1}(\Omega^a))$ such that for all times $t \in (0, T)$

$$\left\langle \frac{1}{c^2} \ddot{\psi}, w \right\rangle_{\Omega^a} + a_a(\psi, w) = l_a(w), \quad w \in X^a, \quad (18)$$

in addition with the initial conditions (17c), where $a_a(\psi, w) = a_{a,1}(\psi, w) + a_{a,2}(\psi, w)$ is splitted into one part deriving from the linear wave operator and another, which arrives from the nonlinear aspect

$$\begin{aligned} a_{a,1}(\psi, w) &= (\nabla\psi, \nabla w)_{\Omega^a}, \\ a_{a,2}(\psi, w) &= \left(\frac{b}{c^2} \nabla\dot{\psi}, \nabla w \right)_{\Omega^a} - \left\langle \frac{B/A}{c^4} \ddot{\psi}, \dot{\psi} w \right\rangle_{\Omega^a} - \left(\frac{2}{c^2} \nabla\dot{\psi}, \nabla\psi w \right)_{\Omega^a}. \end{aligned}$$

The linear functional is similarly defined as

$$\begin{aligned} l_a(w) &= l_{a,1}(w) + l_{a,2}(w) \\ &= \langle g, w \rangle_{\Gamma_N} + \langle \dot{g}, w \rangle_{\Gamma_N}. \end{aligned}$$

2.4 Linear acoustic waves

The Kuznetsov equation (17a) easily allows a connection to the linear wave equation

$$\frac{1}{c^2}\psi_{tt} - \Delta\psi = 0 \quad \text{in } \Omega^a \times (0, T),$$

by setting the right hand side to zero. Hence, we have in (18) the bilinear form $a_a^{\text{lin}}(\cdot, \cdot) = a_{a,1}(\cdot, \cdot)$ and the right hand side $l_a^{\text{lin}}(\cdot) = l_{a,1}(\cdot)$.

3 Coupled systems

In the following, the coupled problem of elasto-acoustics is presented. We first focus on the interface conditions, where the time derivative of the Dirichlet data from one side is coupled with the Neumann data from the other side. After that, we observe how these conditions enter into the variational formulation. Subsequent to the continuous weak formulation, the semi-discrete problem obtained after spatial discretization is presented.

3.1 Structure-acoustic interface

At a solid-fluid interface Γ , as depicted in Figure 1(a), the continuity requires that the normal component of the mechanical surface velocity of the solid must coincide with the normal component of the acoustic velocity of the fluid. Thus, the following relation between the velocity \mathbf{v}_e of the solid expressed by the mechanical displacement \mathbf{u} and the acoustic particle velocity \mathbf{v}_a expressed by the acoustic scalar potential ψ arises:

$$0 = (\mathbf{v}_e - \mathbf{v}_a) \cdot \mathbf{n} = \mathbf{u}_t \cdot \mathbf{n} + \nabla\psi \cdot \mathbf{n} \quad \text{on } \Gamma \times (0, T), \quad (19)$$

where the unit normal vector field \mathbf{n} on Γ points outward of Ω^e . In addition, one has to consider the fact that the ambient fluid causes a surface force $\mathbf{f}_\Gamma = -p_a\mathbf{n} = -\rho_a\psi_t\mathbf{n}$, see (16), which acts like a pressure load on the solid. Therefore, a second coupling condition is given by

$$FS\mathbf{n} + \rho_a\psi_t\mathbf{n} = \mathbf{0} \quad \text{on } \Gamma \times (0, T). \quad (20)$$

3.2 Coupled field formulation

Let us consider a setup of a coupled mechanical-acoustic problem as shown in Figure 1(b), where at the interface Γ we have to consider the solid-fluid coupling. Now, within the domain Ω^e the initial boundary value problem (14) for the mechanical field, within the domain Ω^a the initial boundary value problem (17) for the acoustic field, and along the interface Γ the coupling conditions according to (19) and (20) have to be satisfied. Transforming to the weak form, assuming that homogeneous Neumann data is given on Γ^a , we obtain for the mechanical system

$$\langle \rho_e \ddot{\mathbf{u}}, \mathbf{v} \rangle_{\Omega^e} + a_e(\mathbf{u}, \mathbf{v}) - \langle \mathbf{v}, FS\mathbf{n} \rangle_\Gamma = l_e(\mathbf{v}), \quad (21)$$

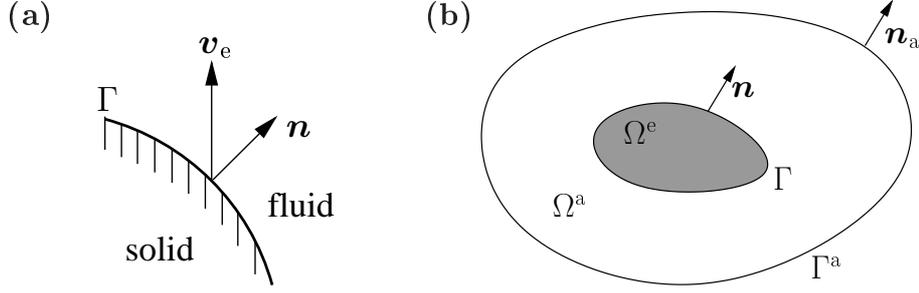


Figure 1: (a) Solid-fluid interface, (b) setup of the coupled elasto-acoustic problem.

and for the acoustic system

$$\left\langle \frac{1}{c^2} \ddot{\psi}, w \right\rangle_{\Omega^a} + a_a(\psi, w) + \langle w, \nabla \psi \cdot \mathbf{n} \rangle_{\Gamma} + \langle w, \overbrace{\gamma_0 \nabla \psi \cdot \mathbf{n}}^{\dot{}} \rangle_{\Gamma} = 0. \quad (22)$$

It should be noted that the plus sign in (22) in front of the first boundary integral over Γ is due to the choice of \mathbf{n} to point outward with respect to the structure Ω^e , see Figure 1(b). Incorporating the coupling conditions (19) and (20), we arrive at the following coupled system of equations

$$\langle \rho_e \ddot{\mathbf{u}}, \mathbf{v} \rangle_{\Omega^e} + a_e(\mathbf{u}, \mathbf{v}) + \langle \rho_a \mathbf{v} \cdot \mathbf{n}, \overbrace{\gamma_0 \psi}^{\dot{}} \rangle_{\Gamma} = l_e(\mathbf{v}), \quad (23)$$

$$\left\langle \frac{1}{c^2} \ddot{\psi}, w \right\rangle_{\Omega^a} + a_a(\psi, w) - \langle w, \overbrace{\gamma_0 \mathbf{u} \cdot \mathbf{n}}^{\dot{}} \rangle_{\Gamma} - \langle w, \overbrace{\gamma_0 \mathbf{u} \cdot \mathbf{n}}^{\ddot{}} \rangle_{\Gamma} = 0. \quad (24)$$

Before we perform a domain discretization, we multiply (24) by ρ_a in order to obtain a boundary integral similar to the one in (23). Thus, the matrices, occurring from a finite element discretization of these two boundary integrals, will be the negative transpose of each other. We finally arrive at the variational problem of finding $(\mathbf{u}, \psi) \in L^2(0, T; X^e \times X^a)$ such that for all times $t \in (0, T)$:

$$\langle \rho_e \ddot{\mathbf{u}}, \mathbf{v} \rangle_{\Omega^e} + a_e(\mathbf{u}, \mathbf{v}) + \langle \rho_a \mathbf{v} \cdot \mathbf{n}, \overbrace{\gamma_0 \psi}^{\dot{}} \rangle_{\Gamma} = l_e(\mathbf{v}), \quad \mathbf{v} \in X^e, \quad (25a)$$

$$\left\langle \frac{\rho_a}{c^2} \ddot{\psi}, w \right\rangle_{\Omega^a} + a_a(\psi, \rho_a w) - \langle \rho_a w, \overbrace{\gamma_0 \mathbf{u} \cdot \mathbf{n}}^{\dot{}} \rangle_{\Gamma} - \langle \rho_a w, \overbrace{\gamma_0 \mathbf{u} \cdot \mathbf{n}}^{\ddot{}} \rangle_{\Gamma} = 0, \quad w \in X^a. \quad (25b)$$

Our main focus in this paper concentrates on the nonlinear elastic/linear acoustic system on the one hand and on the linear elastic/nonlinear acoustic system on the other. The problem formulations do not differ essentially from (25) because nearly all of the nonlinear effects are hidden in the definition of $a_e(\cdot, \cdot)$ and $a_a(\cdot, \cdot)$.

Nonlinear Elastic / Linear Acoustic System

Find $(\mathbf{u}, \psi) \in L^2(0, T; X^e \times X^a)$, $(\dot{\mathbf{u}}, \dot{\psi}) \in L^2(0, T; L^2(\Omega^e) \times L^2(\Omega^a))$, and $(\ddot{\mathbf{u}}, \ddot{\psi}) \in L^2(0, T; H^{-1}(\Omega^e) \times H^{-1}(\Omega^a))$, such that for all times $t \in (0, T)$:

$$\langle \rho_e \ddot{\mathbf{u}}, \mathbf{v} \rangle_{\Omega^e} + a_e(\mathbf{u}, \mathbf{v}) + \langle \rho_a \mathbf{v} \cdot \mathbf{n}, \overbrace{\dot{\gamma}_0 \psi} \rangle_{\Gamma} = l_e(\mathbf{v}), \quad \mathbf{v} \in X^e, \quad (26a)$$

$$\langle \frac{\rho_a}{c^2} \ddot{\psi}, w \rangle_{\Omega^a} + a_a^{\text{lin}}(\psi, \rho_a w) - \langle \rho_a w, \overbrace{\dot{\gamma}_0 \mathbf{u} \cdot \mathbf{n}} \rangle_{\Gamma} = 0, \quad w \in X^a. \quad (26b)$$

Linear Elastic / Nonlinear Acoustic System

Find $(\mathbf{u}, \psi) \in L^2(0, T; X^e \times X^a)$, $(\dot{\mathbf{u}}, \dot{\psi}) \in L^2(0, T; L^2(\Omega^e) \times L^2(\Omega^a))$, and $(\ddot{\mathbf{u}}, \ddot{\psi}) \in L^2(0, T; H^{-1}(\Omega^e) \times H^{-1}(\Omega^a))$, such that for all times $t \in (0, T)$:

$$\langle \rho_e \ddot{\mathbf{u}}, \mathbf{v} \rangle_{\Omega^e} + a_e^{\text{lin}}(\mathbf{u}, \mathbf{v}) + \langle \rho_a \mathbf{v} \cdot \mathbf{n}, \overbrace{\dot{\gamma}_0 \psi} \rangle_{\Gamma} = l_e(\mathbf{v}), \quad \mathbf{v} \in X^e, \quad (27a)$$

$$\langle \frac{\rho_a}{c^2} \ddot{\psi}, w \rangle_{\Omega^a} + a_a(\psi, \rho_a w) - \langle \rho_a w, \overbrace{\dot{\gamma}_0 \mathbf{u} \cdot \mathbf{n}} \rangle_{\Gamma} - \langle \rho_a w, \overbrace{\ddot{\gamma}_0 \mathbf{u} \cdot \mathbf{n}} \rangle_{\Gamma} = 0, \quad w \in X^a. \quad (27b)$$

We remark that an alternative coupled problem can be derived, if, instead of the potential-based formulation, a displacement-based problem formulation is chosen also for the fluid domain. A rigorous mathematical error analysis for the purely linear case is provided in [2] for the case of matching grids which could be extended to the non-matching situation. There, due to the displacement-based formulation, the weak form of the sub-problem for the fluid is an H^{div} -problem requiring a non-standard discretization by means of Raviart–Thomas finite elements. Here, we are able to use standard Lagrangian nodal finite elements in both domains.

3.3 Discretization

For the following considerations, the notation sets up on [12], in combination with [1, 6]. For the time integration of nonlinear structural dynamics, we will consider the generalized α -method, which extends Newmark's method by introducing two additional parameters $\alpha_m, \alpha_f \in [0, 1]$ and setting

$$\ddot{\mathbf{u}}_{n+1-\alpha_m} = (1 - \alpha_m) \ddot{\mathbf{u}}_{n+1} + \alpha_m \ddot{\mathbf{u}}_n, \quad \dot{\mathbf{u}}_{n+1-\alpha_f} = (1 - \alpha_f) \dot{\mathbf{u}}_{n+1} + \alpha_f \dot{\mathbf{u}}_n, \quad (28a)$$

$$\mathbf{u}_{n+1-\alpha_f} = (1 - \alpha_f) \mathbf{u}_{n+1} + \alpha_f \mathbf{u}_n, \quad \mathbf{f}_{n+1-\alpha_f} = (1 - \alpha_f) \mathbf{f}_{n+1} + \alpha_f \mathbf{f}_n. \quad (28b)$$

Applying (28) to nonlinear structural dynamics on the spatially discrete level yields the system

$$M_e \ddot{\mathbf{u}}_{n+1-\alpha_m} + C_e \dot{\mathbf{u}}_{n+1-\alpha_f} + N_e(\mathbf{u}_{n+1-\alpha_f}) = \mathbf{f}_{n+1-\alpha_f},$$

with the constant mass matrix M_e , the constant damping matrix C_e , the internal forces N_e , and the external load \mathbf{f} .

Setting $a_1 = (1 - \alpha_f)\gamma/(\beta\Delta t)$ and $a_2 = (1 - \alpha_m)/(\beta\Delta t^2)$, the generalized mid-point velocities and accelerations can be given as functions of the end-point displacements \mathbf{u}_{n+1} by

$$\dot{\mathbf{u}}_{n+1-\alpha_f}(\mathbf{u}_{n+1}) = a_1\mathbf{u}_{n+1} - \widehat{\dot{\mathbf{u}}}_n, \quad (29a)$$

$$\widehat{\dot{\mathbf{u}}}_n = a_1\mathbf{u}_n + \frac{(1 - \alpha_f)\gamma - \beta}{\beta}\dot{\mathbf{u}}_n + \frac{(1 - \alpha_f)(\gamma - 2\beta)}{2\beta}\Delta t\ddot{\mathbf{u}}_n, \quad (29b)$$

$$\ddot{\mathbf{u}}_{n+1-\alpha_m}(\mathbf{u}_{n+1}) = a_2\mathbf{u}_{n+1} - \widehat{\ddot{\mathbf{u}}}_n, \quad (29c)$$

$$\widehat{\ddot{\mathbf{u}}}_n = a_2\mathbf{u}_n + \frac{1 - \alpha_m}{\beta\Delta t}\dot{\mathbf{u}}_n + \frac{1 - \alpha_m - 2\beta}{2\beta}\ddot{\mathbf{u}}_n. \quad (29d)$$

This gives the effective structural equation

$$\mathbf{0} = \widetilde{F}_e(\mathbf{u}_{n+1}) = N_e(\mathbf{u}_{n+1-\alpha_f}) - \mathbf{f}_{n+1-\alpha_f} + C_e\dot{\mathbf{u}}_{n+1-\alpha_f}(\mathbf{u}_{n+1}) + M_e\ddot{\mathbf{u}}_{n+1-\alpha_m}(\mathbf{u}_{n+1}). \quad (30)$$

The application of Newton's method to (30) amounts to solve in each iteration step q the linear system

$$K_e^*(\mathbf{u}_{n+1}^q)\Delta\mathbf{u} = -\widetilde{F}_e(\mathbf{u}_{n+1}^q), \quad \Delta\mathbf{u} = \mathbf{u}_{n+1}^{q+1} - \mathbf{u}_{n+1}^q,$$

with the deformation-dependent effective tangential matrix $K_e^*(\mathbf{u}_{n+1}^q)$ given by

$$K_e^*(\mathbf{u}_{n+1}^q) = K_{n+1-\alpha_m}^t(\mathbf{u}_{n+1}^q) + a_1C_e + a_2M_e, \quad (31)$$

where $K_{n+1-\alpha_m}^t(\mathbf{u}_{n+1}^q)$ denotes the tangential stiffness matrix

$$K_{n+1-\alpha_m}^t(\mathbf{u}_{n+1}^q) = \frac{\partial N_e(\mathbf{u}_{n+1-\alpha_f}^q)}{\partial \mathbf{u}_{n+1}}. \quad (32)$$

The generalized α -method applied to the weak form (27b) of the wave equation (17a) for the acoustic velocity potential ψ gives

$$M_a\ddot{\psi}_{n+1-\alpha_m} + C_a\dot{\psi}_{n+1-\alpha_f} + K_a\psi_{n+1-\alpha_f} = N_1(\dot{\psi}_{n+1-\alpha_f})\ddot{\psi}_{n+1-\alpha_m} + N_2(\psi_{n+1-\alpha_f})\dot{\psi}_{n+1-\alpha_f}, \quad (33)$$

with constant matrices M_a, C_a, K_a and

$$[N_1(\dot{\psi})]_{ij} = \int_{\Omega^a} \frac{B/A}{c^2} \phi_i \phi_j \sum_r \phi_r \dot{\psi}_r, \quad [N_2(\psi)]_{ij} = \int_{\Omega^a} 2\phi_i \nabla \phi_j \cdot \sum_r \nabla \phi_r \psi_r. \quad (34)$$

Here, ϕ_r denotes the standard nodal basis functions for the acoustic potential ψ associated with the node r . Similar as for the elastic part, we have to solve a linear system in each time step

$$K_a^*\psi_{n+1} = C_a\widehat{\dot{\psi}}_n + M_a\widehat{\ddot{\psi}}_n + N_a(\psi_{n+1}),$$

where $N_a(\psi_{n+1})$ denotes the Newmark representation of the right hand side in (33) and

$$K_a^* = K_a + a_1C_a + a_2M_a.$$

This gives the effective acoustical equation

$$0 = \widetilde{F}_a(\psi_{n+1}) = K_a^*\psi_{n+1} - C_a\widehat{\dot{\psi}}_n - M_a\widehat{\ddot{\psi}}_n - N_a(\psi_{n+1}).$$

3.4 The global systems

We set $u = (\mathbf{u}, \psi)^\top$ and the matrices

$$K = \begin{pmatrix} K_e & 0 \\ 0 & K_a \end{pmatrix}, C = \begin{pmatrix} C_e & C_{ea} \\ -C_{ea}^\top & C_a \end{pmatrix}, M = \begin{pmatrix} M_e & 0 \\ M_{ae} & M_a \end{pmatrix}, \quad (35)$$

and the effective stiffness matrix

$$K^* = K + a_1 C + a_2 M. \quad (36)$$

Furthermore let us define

$$\tilde{u}_n = C\hat{u}_n + M\hat{u}_n. \quad (37)$$

Finally we arrived at our fully discrete systems:

Nonlinear Elastic / Linear Acoustic Discrete System

The global discrete system coupling nonlinear structural dynamics with linear acoustics reads

$$0 = F(u_{n+1}) = \begin{pmatrix} F_e(u_{n+1}) \\ F_a(u_{n+1}) \end{pmatrix} = \begin{pmatrix} N_e(\mathbf{u}_{n+1-\alpha_f}) \\ K_a \psi_{n+1} \end{pmatrix} + (a_1 C + a_2 M)u_{n+1} - \tilde{u}_n - \begin{pmatrix} \mathbf{f}_{n+1-\alpha_f} \\ 0 \end{pmatrix}. \quad (38)$$

Linear Elastic / Nonlinear Acoustic Discrete System

The global discrete system coupling linear structural dynamics with nonlinear acoustics reads

$$0 = F(u_{n+1}) = \begin{pmatrix} F_e(u_{n+1}) \\ F_a(u_{n+1}) \end{pmatrix} = K^* u_{n+1} - \tilde{u}_n - \begin{pmatrix} \mathbf{f}_{n+1-\alpha_f} \\ N_a(\psi_{n+1}) \end{pmatrix}. \quad (39)$$

Now, we have derived the requested form (1) of different nonlinearities in structure-acoustic interaction application. It remains to show, that the theory of Section 1 can be applied to the systems (38) and (39). This will be done in the following two statements.

Lemma 3.1. *The Assumptions (A1)-(A3) hold for F defined by (38) and the decomposition introduced above.*

Proof. By the definition of F in (38), the Jacobian $J(u)$ is given by

$$J(u) = \begin{pmatrix} K_e^*(\mathbf{u}) & \tilde{B}^\top \\ -\tilde{B} & K_a^* \end{pmatrix},$$

with $K_e^*(\mathbf{u})$ and K_a^* defined by (31) and (36), respectively, and $\tilde{B}^T = a_1 C_{ea}$. Being constant, it is obvious that K_a^* and \tilde{B} are continuous. Moreover, due to the use of the geometrically nonlinear elasticity model (12)–(14a), the effective tangent matrix $K_e^*(\mathbf{u})$ is given in terms of polynomials of the gradient $\text{grad } \mathbf{u}$, and is also continuous, which proves (A1). The subdomain matrices $E_i J(u^*) E_i^T$, $i = e, a$, are given by $K_e^*(\mathbf{u})$ and K_a^* , respectively. Since one component is the multiple $a_2 M_i$ with M_i being the corresponding mass matrix and with $a_2 = O(\Delta t^{-2})$, both matrices are positive definite for Δt small enough, provided that $\alpha_m < 1$ and $\beta > 0$, regardless of the underlying boundary conditions. This shows (A3). In order to investigate the regularity of the global Jacobian $J(u^*)$, we split the degrees of freedom associated with the acoustic potential ψ into (ψ_I, ψ_Γ) corresponding to the interior nodes and the interface nodes, respectively. This allows to decompose $J(u)$ into

$$J(u) = \begin{pmatrix} K_e^*(\mathbf{u}) & 0 & B^T \\ 0 & K_{II} & K_{I\Gamma} \\ -B & K_{\Gamma I} & K_{\Gamma\Gamma} \end{pmatrix}, \quad (40)$$

with the obvious meanings for the newly introduced submatrices. We note that in order to analyze the regularity of $J(u)$ within the framework of saddle point problems, the matrix $\tilde{B}^T = (0 \ B^T)$ would have to satisfy an inf-sup condition of the form

$$\|\tilde{B}^T \psi\| \geq \tilde{\beta} \|\psi\|, \quad \psi \in \mathbb{R}^{m_a},$$

which clearly is not the case (take $\psi = (\psi_I, 0)^T$). However, by means of the Schur complement $S_a = K_{\Gamma\Gamma} - K_{\Gamma I} K_{II}^{-1} K_{I\Gamma}$, we can equivalently reformulate the system $J(u) = g$ as $\tilde{J}(u) = \tilde{g}$ with

$$\tilde{J}(u) = \begin{pmatrix} K_e^*(\mathbf{u}) & B^T \\ -B & S_a \end{pmatrix}. \quad (41)$$

Now, the matrix B^T is well understood within the framework of mortar finite elements, [3, 4], and, in the case of the employed discretization, is known to satisfy the required inf-sup condition, namely, there exists $\beta > 0$ such that

$$\|B^T \psi_\Gamma\| \geq \beta \|\psi_\Gamma\|, \quad \psi_\Gamma \in \mathbb{R}^{m_\Gamma}.$$

Furthermore, the effective tangent matrix $K_e^*(\mathbf{u})$ is positive definite as justified above, and the Schur complement S_a of the positive definite matrix K_a^* is itself positive definite. Thus, the standard saddle point theory, [5], can be applied to (41), yielding the regularity of $\tilde{J}(u)$, and, therefore, of $J(u)$, which justifies (A2). \square

Lemma 3.2. *The Assumptions (A1)–(A3) hold for F defined by (39) and the decomposition introduced above.*

Proof. We can alter the proof in order to use it for the linear elastic / nonlinear acoustic problem (39). We follow the argumentation of the nonlinear elasticity concept except of defining J as

$$J(u) = \begin{pmatrix} K_e^* & K_{ea}^* \\ K_{ae}^* & K_a^* - JN_a(\psi) \end{pmatrix},$$

with $JN_a(\psi)$ being the Jacobian of $N_a(\psi)$. From definition (34) we see that N_a depends continuously on ψ and $\nabla\psi$. Together with the fact that the effective stiffness matrix K^* is constant, condition (A1) is fulfilled. Furthermore, we set

$$\begin{aligned}\tilde{B}^T &= K_{ea}^* = a_1 C_{ea}, \\ K_{ae}^* &= -a_1 C_{ea}^T + a_2 M_{ae}.\end{aligned}$$

For the Kuznetsov equation, we have $M_{ae} = -\frac{b}{c^2} C_{ea}^T$ and hence

$$K_{ae}^* = -\left(1 + \frac{a_2 b}{a_1 c^2}\right) \tilde{B}.$$

We now define $K_a^*(\psi) = K_a^* - JN_a(\psi)$, which leads to the Jacobian

$$J(u) = \begin{pmatrix} K_e^* & \tilde{B}^T \\ -\left(1 + \frac{a_2 b}{a_1 c^2}\right) \tilde{B} & K_a^*(\psi) \end{pmatrix}.$$

Decompose \mathbf{u} into $(\mathbf{u}_I, \mathbf{u}_\Gamma)$, then

$$J(u) = \begin{pmatrix} K_{II} & K_{I\Gamma} & 0 \\ K_{\Gamma I} & K_{\Gamma\Gamma} & \tilde{B}^T \\ 0 & -\left(1 + \frac{a_2 b}{a_1 c^2}\right) \tilde{B} & K_a^*(\psi) \end{pmatrix}.$$

Here we can simply divide the last line and the corresponding right hand side by $(1 + \frac{a_2 b}{a_1 c^2})$. The Schur complement $S_a = K_{\Gamma\Gamma} - K_{\Gamma I} K_{II}^{-1} K_{I\Gamma}$ leads to the matrix

$$\tilde{J}(u) = \begin{pmatrix} S_a & B^T \\ -B & K_a^*(\psi) \end{pmatrix},$$

for which the same arguments as for (41) hold. \square

Remark 3.3. The global Jacobian $J(u)$ could also be analyzed directly within the framework of generalized saddle point problems, [7]. In particular, (40) has the structure

$$\begin{pmatrix} A & B_1^T \\ -B_2 & C \end{pmatrix},$$

with $A = \text{diag}(K_e^*(\mathbf{u}), K_{II})$, $B_1 = (B, K_{\Gamma I})$, $B_2 = (B, -K_{\Gamma I})$, $C = K_{\Gamma\Gamma}$. However, the regularity could only be guaranteed provided that the contraction factor of a corresponding fix point mapping involving the continuity and ellipticity constants would be sufficiently small. With the problem adapted proof given above, it is not necessary to deal with this contraction factor.

3.5 The iterative solution procedures

We present the overall iterative solution procedure for system (38) in Algorithm 1 and for system (39) in Algorithm 2. The essential algorithmic difference is that we use Newton's method for the resolution of the nonlinear elastic subproblem, while we employ a fixed point iteration for the nonlinear acoustic part.

Algorithm 1 Iterative solution by a nonlinearly preconditioned Richardson scheme

```

Set up the matrices  $M, C, K_a, K_a^*$ . (35),(36)
for all time steps  $n = 1, \dots$  do
  Calculate  $\mathbf{f}, \hat{u}, \tilde{u}, \tilde{u}$ . (29b),(29d),(37)
  for all Richardson steps  $k = 1, \dots$  do
    for all Newton steps  $q = 1, \dots$  do
      Calculate  $K^t(\mathbf{u}), K_e^*(\mathbf{u}), F_e(u)$ . (32),(31),(38)
      Solve  $K_e^* \Delta \mathbf{u} = -F_e(u)$ .
      Update  $\mathbf{u} \leftarrow \mathbf{u} + \Delta \mathbf{u}$ .
      Check for Newton convergence.
    end for
    Calculate  $\hat{g} = \tilde{\psi} + a_1 C_{ea}^T \mathbf{u}$ .
    Solve  $K_a^* \psi = \hat{g}$ .
    Update  $u$ . (4)
    Check for Richardson convergence.
  end for
  Update  $\dot{u}, \ddot{u}$ . (29a),(29c)
end for

```

For system (38) we remark that most of the matrices only have to be assembled once in the very beginning, and only the relatively small tangential stiffness matrix $K^t(\mathbf{u})$ has to be calculated in every Newton step. The only difference between the additive and the multiplicative variant is the update of the displacement degrees of freedom before the solution for the new velocity potential in the latter case. Thus, as in the linear case, for single processor architectures, the costs per iteration step are almost the same, and the multiplicative variant is clearly superior to the additive one. As is well-known, this argument has to be reconsidered in the case of parallel computing architectures.

4 Numerical computations

We provide several numerical results illustrating the applicability and efficiency of our approach. In particular, we validate our theoretical results in Section 4.1, and discuss some further improvements in Sections 4.2 and 4.3.

Algorithm 2 Iterative solution by a nonlinearly preconditioned Richardson scheme

Set up the matrices M, C, K, K^* . (35),(36)

for all time steps $n = 1, \dots$ **do**

 Calculate $\mathbf{f}, \hat{u}, \hat{u}, \tilde{u}$. (29b),(29d),(37)

for all Richardson steps $k = 1, \dots$ **do**

 Calculate $\hat{\mathbf{f}} = \mathbf{f} + \tilde{\mathbf{u}} - a_1 C_{\text{ea}} \psi$.

 Solve $K_e^* \mathbf{u} = \hat{\mathbf{f}}$.

for all Fixed point iteration steps $q = 1, \dots$ **do**

 Calculate $N(\psi, \dot{\psi}, \ddot{\psi}) = N_1(\dot{\psi})\ddot{\psi} + N_2(\psi)\dot{\psi}$. (34)

 Solve $K_a^* \psi = \tilde{\psi} + N(\psi, \dot{\psi}, \ddot{\psi}) + a_1 C_{\text{ea}}^T \mathbf{u} - a_2 M_{\text{ae}} \mathbf{u}$. (4),(29a),(29c)

 Update $\psi, \dot{\psi}, \ddot{\psi}$. (4),(29a),(29c)

 Check for Fixed point convergence.

end for

 Update u, \dot{u}, \ddot{u} . (4),(29a),(29c)

 Check for Richardson convergence.

end for

end for

4.1 Validation of the theoretical results

In the following, we investigate Theorems 1.2 and 1.7 by means of a numerical example simulating the sound emission of a vibrating structure in water. The structure Ω^e is of width 0.2 m and height 0.01 m and has the material parameters of silicon, $\rho_e = 2.3 \cdot 10^3 \text{ kg m}^{-3}$, $E = 1.62 \cdot 10^{11} \text{ N m}^{-2}$, $\nu = 0.2$. It is fixed at its left and right boundary, and a surface traction of $10^8 \sin(2\pi 1000t) \text{ N m}^{-2}$ is acting in vertical direction at its lower boundary. We assume the structure to behave geometrically nonlinear. The acoustic fluid domain Ω^a of width 1.4 m and height 0.7 m is centered above the structure. The mean density is $\rho_a = 10^3 \text{ kg m}^{-3}$, the speed of sound is $c = 1.5 \cdot 10^3 \text{ m s}^{-1}$. The corresponding parameters for the nonlinear wave equation in water are $B/A = 5$ and $b = 1.83 \cdot 10^{-10} \text{ m}^2 \text{ s}^{-1}$. Due to symmetry reasons, we can set the computational domain to one half of the original one, see Figure 2. As described in [10], we are able to use nonmatching grids in the different subdomains. This allows us to be as flexible as possible in the choice of the grids.

A test series with varying damping parameter ω is performed. In each test, 20 time steps of size $2.5 \cdot 10^{-5} \text{ s}$ are carried out. Figures 3(a),(b) show the averaged convergence rate versus the value of ω for the nonlinear scheme (4) and for its linearized variant. We observe that even the averaged convergence rate of the nonlinear iteration, which is directly related to the number of iterations necessary to achieve a desired reduction of the error, is in good agreement with the one of the linear iteration. This nicely confirms and even strengthens the statement of Theorem 1.2. Moreover, for this particular example, a damping parameter $\omega = 0.7$ seems to be optimal. However, the minimum achievable convergence rate of around 0.55 or 0.5 is far too high for a block 2×2 -scheme to be efficient. In the following section, we therefore will gradually improve our iteration scheme.

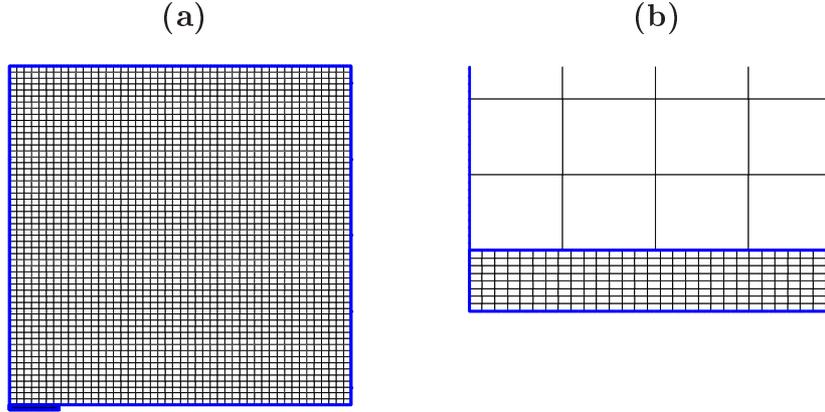


Figure 2: (a) Computational grid: lower small part = structure, upper part = acoustic, (b) use of nonmatching grids.

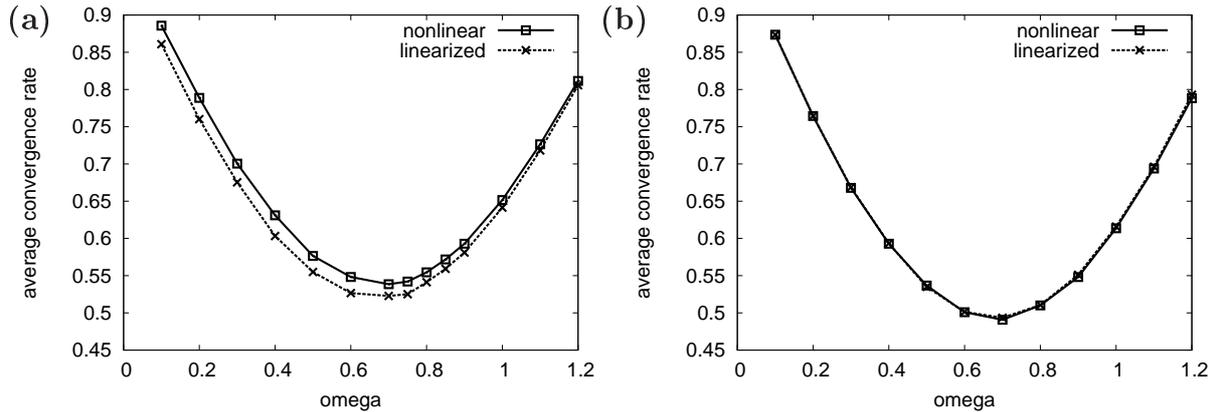


Figure 3: Test of Richardson scheme (4): average convergence rate versus damping parameter (a) for system (38) and (b) for system (39).

We perform the same test series for the multiplicative variant (8) as described above. In Figure 4, the resulting averaged convergence rates are plotted against the damping parameter as before. Additionally, the result for the additive variant from before is given for comparison.

We observe that the nonlinear and the linearized multiplicative variant are in reasonable agreement. However, for the system (38), while the difference to the right of the optimum value is almost not visible, the one to the left becomes quite remarkable. More important, the convergence rates are in general much better than for the Jacobi scheme. It is possible to reach a minimum value of roughly 0.2. Yet, this is still quite high for a block 2×2 -system. We will discuss a further improvement in the next section.

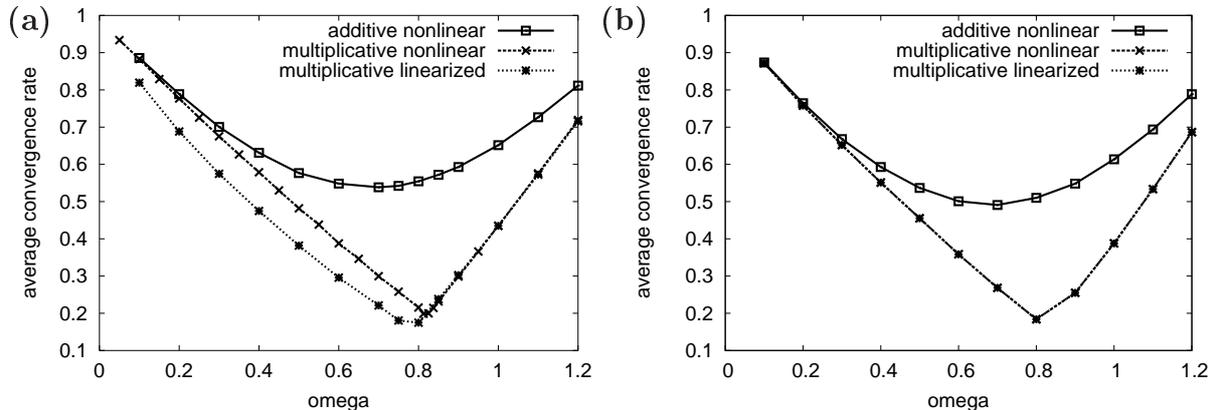


Figure 4: Test of multiplicative variant (8): convergence rate versus damping parameter (a) for system (38) and (b) for system (39).

4.2 Overlapping subdomains

In order to improve the convergence behavior of the Richardson scheme, we further decompose ψ into $(\psi_1, \psi_2, \lambda)$, where \mathbf{u} couples with ψ_1 via C_{ea} , and ψ_1 with ψ_2 via the Lagrange multiplier λ in the manner of mortar finite element methods, [3, 4]. We note that this procedure admits to use nonconforming grids in the acoustic subdomains associated with ψ_1 and ψ_2 . However, we will not exploit this fact in our presentation.

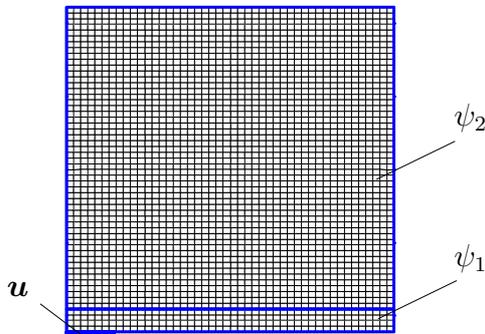


Figure 5: Computational domain with 4 layers overlap.

In Figure 5, the computational grid is plotted, visualizing the structure in the lower left part. The thicker horizontal line inside the acoustic domain indicates the upper boundary of the overlapping region. We first concentrate on system (38). For the effective stiffness matrix associated with Ω^a and arranged with respect to the decomposition into $(\psi_1, \psi_2, \lambda)$, we have

$$K_a^* = \begin{pmatrix} K_{11} & 0 & K_{1\lambda} \\ 0 & K_{22} & K_{2\lambda} \\ K_{\lambda 1} & K_{\lambda 2} & 0 \end{pmatrix} + a_1 \begin{pmatrix} C_1 & 0 & 0 \\ 0 & C_2 & 0 \\ 0 & 0 & 0 \end{pmatrix} + a_2 \begin{pmatrix} M_1 & 0 & 0 \\ 0 & M_2 & 0 \\ 0 & 0 & 0 \end{pmatrix},$$

with the obvious meanings for the submatrices. We now choose a decomposition of $(1, \dots, m)$ into I_e^o and I_a with I_a as before including the indices associated with the Lagrange multiplier λ , but with I_e^o being I_e enhanced by the indices associated with ψ_1 . Now, this decomposition is overlapping, i.e., $|I_e| + |I_a| > m$. The resulting subspace function F_e^o associated with I_e^o is given by

$$F_e^o(u) = P_e^o F(u) = \begin{pmatrix} F_e(u) \\ K_{11}^* \psi_1 - C_{ea}^T \mathbf{u} + K_{1\lambda} \lambda - \tilde{\psi}_1 \end{pmatrix}. \quad (42)$$

We now apply the Richardson iteration (4) to the preconditioned system

$$0 = \mathcal{F}_m^o(u^*) = T_e^o(u^*) + T_a(u^* - T_e^o(u^*)). \quad (43)$$

For the resulting algorithm, only the Newton iteration has to be changed, i.e. the shaded region in Algorithm 1. The modified Newton scheme is given in Algorithm 3.

Algorithm 3 Newton iteration for overlapping scheme

for all Newton steps $q = 1, \dots$ **do**
 Calculate $K^t(\mathbf{u})$, $K_e^*(\mathbf{u})$, $F_e^o(u)$. (32),(31),(42)
 Set up $K_o^* = \begin{pmatrix} K_e^*(\mathbf{u}) & K_{ea}^* \\ K_{ae}^* & K_1^* \end{pmatrix}$.
 Solve $K_o^* \Delta \begin{pmatrix} \mathbf{u} \\ \psi_1 \end{pmatrix} = -F_e^o(u)$.
 Update $\begin{pmatrix} \mathbf{u} \\ \psi_1 \end{pmatrix} \leftarrow \begin{pmatrix} \mathbf{u} \\ \psi_1 \end{pmatrix} + \Delta \begin{pmatrix} \mathbf{u} \\ \psi_1 \end{pmatrix}$.
 Check for Newton convergence.
end for

The goal of this overlapping scheme is to include in I_e^o only comparatively few degrees of freedom from the acoustic part, such that the computational costs for one iteration step are not much higher than for the non-overlapping variant, but to overlap enough to substantially improve the convergence rate.

In the case of the linear elastic/nonlinear acoustic system (39), we also introduce the overlap in the acoustic region. In contrast to Algorithm 3 we solve the linearized acoustic equation, i.e. we only make one fixed point iteration step, on the overlapping region. With the same notations as above we only have to change the equation outside the fixed point iteration in Algorithm 2 as is written in Algorithm 4.

We use the same example as above to investigate the behaviour of the overlapping method. In particular, we vary the thickness of the overlap. In Figures 6(a),(b), the iteration counts for different numbers of overlapping layers are visualized against the time steps. Convergence for the Richardson iteration was declared, when the relative difference of two successive iterates went below 10^{-10} . Already a very small number of layers results in a strong improvement. With four or eight layers, the count is around 5 or 4, which is quite reasonable.

Algorithm 4 Linearized adaption for overlapping scheme

for all Richardson steps $k = 1, \dots$ **do**

 Calculate $N(\psi_1, \dot{\psi}_1, \ddot{\psi}_1)$.

 Perform one fixed point step for solving

$$\begin{pmatrix} K_e^* & K_{ea}^* \\ K_{ae}^* & K_1^* \end{pmatrix} \begin{pmatrix} \mathbf{u} \\ \psi_1 \end{pmatrix} = \begin{pmatrix} \tilde{\mathbf{u}} \\ \tilde{\psi}_1 \end{pmatrix} + \begin{pmatrix} \mathbf{f} \\ N(\psi_1) \end{pmatrix} - \begin{pmatrix} 0 \\ (K_{1\lambda} + a_1 C_{1\lambda})\lambda \end{pmatrix}.$$

 Update $\psi_1, \dot{\psi}_1, \ddot{\psi}_1$.

(4),(29a),(29c)

for all Fixed point iteration steps $q = 1, \dots$ **do**

 ...

end for

 Update u, \dot{u}, \ddot{u} .

(4),(29a),(29c)

 Check for Richardson convergence.

end for

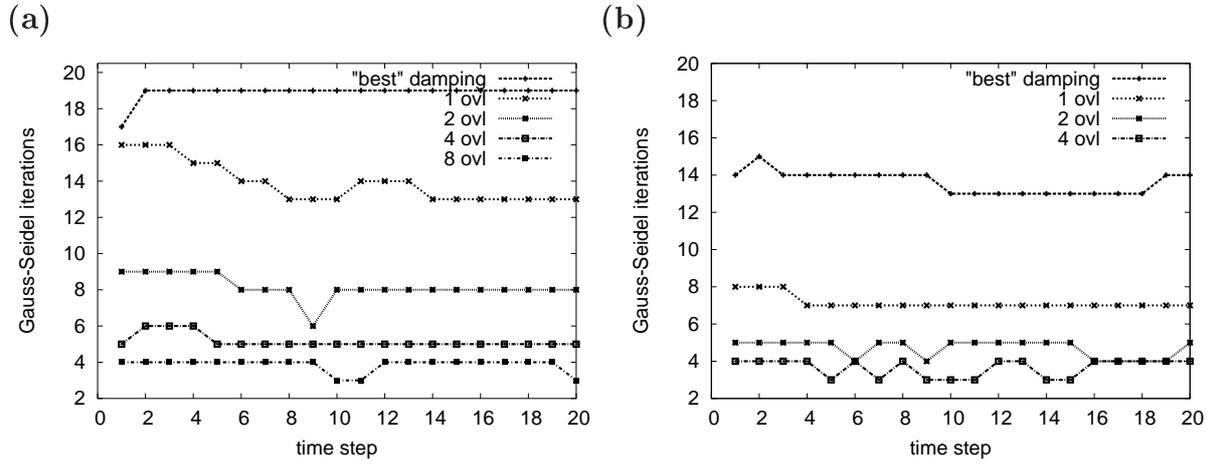


Figure 6: Test of overlapping scheme: iteration count versus time step, varying the overlap (a) for system (38) and (b) for system (39).

4.3 An inexact strategy

For the system (26), so far, in each Richardson step, there have been made so many Newton steps as necessary to meet the stopping criteria of the relative difference of two iterates to be below 10^{-10} . In Figure 7, the number of Newton iterations is plotted versus the time step for the multiplicative scheme using four layers of overlap. In particular, the total number of Newton iterations per time step determines the height of the columns, whereas each column is subdivided to display the number of Newton iterations per Richardson step within each time step. The first observation to be made is that the total number of Newton iterations per time step is almost constant, as already suggested by the stable behaviour of the multiplicative scheme. Moreover, the number of Newton iterations in each Richardson step is very low. Starting from the solution of the previous time step, it only takes four

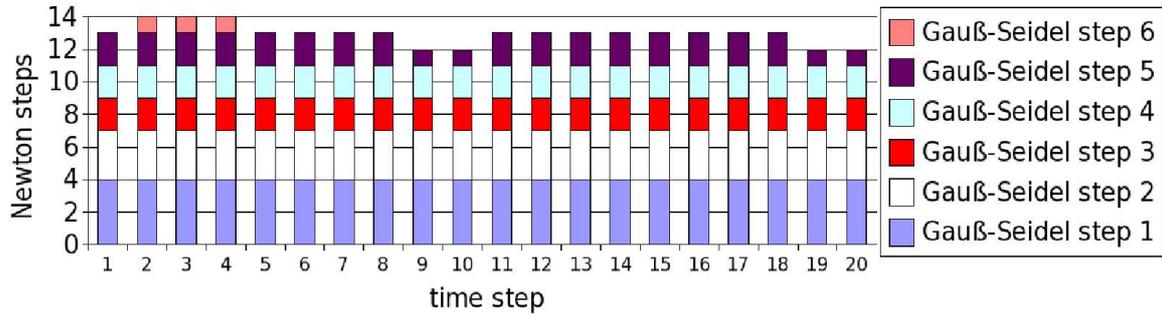


Figure 7: Overlapping multiplicative scheme, four layers of overlap: Newton iterations versus time step.

Newton iterations in the first Richardson step, three in the second, and between one and two in the subsequent steps. Nevertheless, the efficiency of the scheme can further be improved by employing an inexact strategy.

To this end, only one single Newton step is performed in each Richardson step. Figure 8 shows the resulting iteration count for the multiplicative scheme versus the time steps for different numbers of overlapping layers.

Up to eight layers, almost no difference between the exact and the inexact method can be observed. This means that the number of Newton steps per time step reduces significantly to the number of Richardson steps per time step. We remark that the resulting number of Newton steps per time step for the inexact strategy seems to be bounded from below by the number of Newton steps for the first Richardson step of the exact strategy. Thus, if the size of the overlap further increases, the iteration count for the inexact method becomes worse than the one for the exact method. However, in the reasonable range between four and eight layers of overlap, the inexact strategy is clearly superior.

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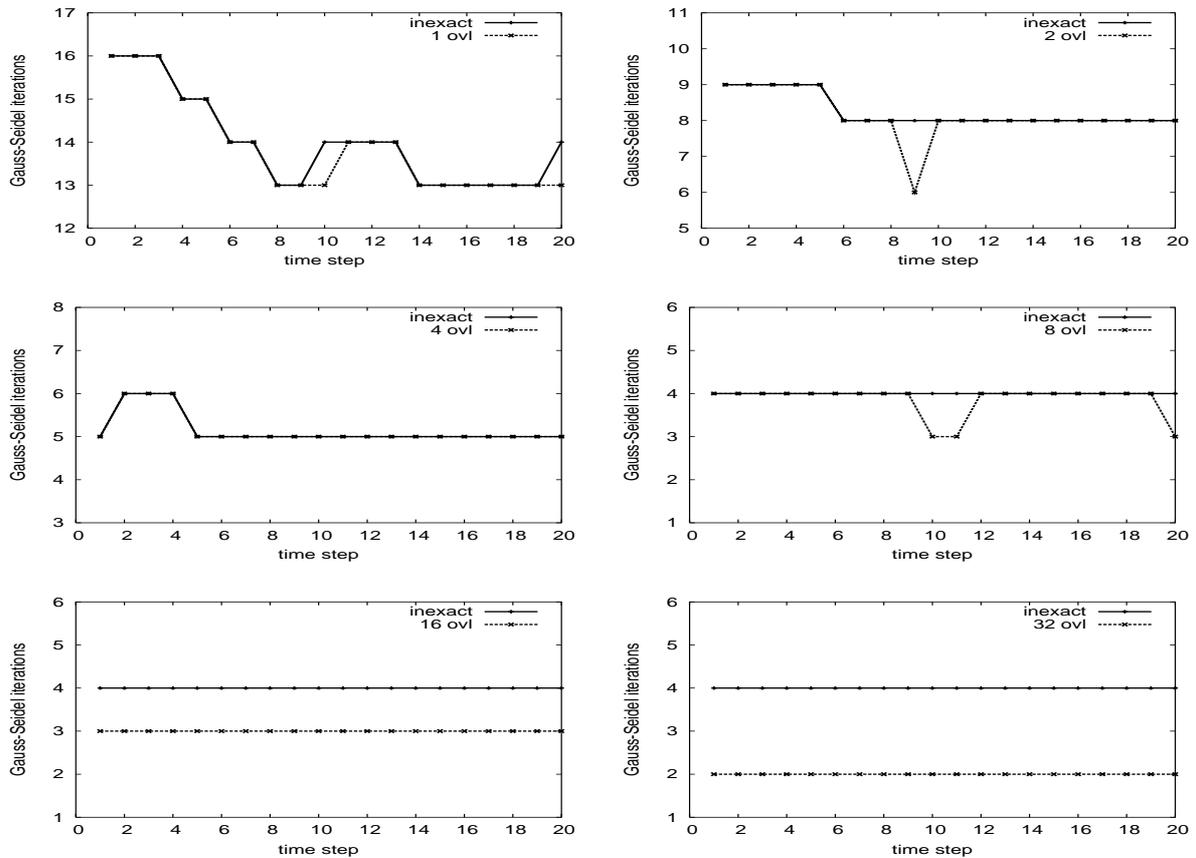


Figure 8: Overlapping multiplicative scheme: inexact (solid line) vs. exact (dashed) strategy.

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